Freescale Semiconductor

Technical Data

Document Number: MRF1513N

Rev. 10, 2/2008

√RoHS

RF Power Field Effect Transistor

N-Channel Enhancement-Mode Lateral MOSFET

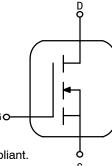
Designed for broadband commercial and industrial applications with frequencies to 520 MHz. The high gain and broadband performance of this device make it ideal for large-signal, common source amplifier applications in 7.5 volt portable and 12.5 volt mobile FM equipment.

Specified Performance @ 520 MHz, 12.5 Volts
 Output Power — 3 Watts
 Power Gain — 11 dB
 Efficiency — 55%

 Capable of Handling 20:1 VSWR, @ 15.5 Vdc, 520 MHz, 2 dB Overdrive

Features

- Excellent Thermal Stability
- Characterized with Series Equivalent Large-Signal Impedance Parameters
- N Suffix Indicates Lead-Free Terminations. RoHS Compliant.
- In Tape and Reel. T1 Suffix = 1,000 Units per 12 mm, 7 Inch Reel.



MRF1513NT1

520 MHz, 3 W, 12.5 V LATERAL N-CHANNEL BROADBAND RF POWER MOSFET



Table 1. Maximum Ratings

Rating	Symbo	l Value	Unit
Drain-Source Voltage	V _{DSS}	-0.5, +40	Vdc
Gate-Source Voltage	V _{GS}	±20	Vdc
Drain Current — Continuous	I _D	2	Adc
Total Device Dissipation @ T _C = 25°C ⁽¹⁾ Derate above 25°C	P _D	31.25 0.25	W W/°C
Storage Temperature Range	T _{stg}	- 65 to +150	°C
Operating Junction Temperature	TJ	150	°C

Table 2. Thermal Characteristics

	Characteristic	Symbol	Value ⁽²⁾	Unit
The	ermal Resistance, Junction to Case	$R_{ heta JC}$	4	°C/W

Table 3. Moisture Sensitivity Level

Test Methodology	Rating	Package Peak Temperature	Unit
Per JESD 22-A113, IPC/JEDEC J-STD-020		260	°C

- 1. Calculated based on the formula $P_D = \frac{T_J T_C}{R_{\theta J C}}$
- 2. MTTF calculator available at http://www.freescale.com/rf. Select Software & Tools/Development Tools/Calculators to access MTTF calculators by product.

NOTE - <u>CAUTION</u> - MOS devices are susceptible to damage from electrostatic charge. Reasonable precautions in handling and packaging MOS devices should be observed.



Table 4. Electrical Characteristics ($T_C = 25^{\circ}C$ unless otherwise noted)

Characteristic	Symbol	Min	Тур	Max	Unit
Off Characteristics					
Zero Gate Voltage Drain Current (V _{DS} = 40 Vdc, V _{GS} = 0 Vdc)	I _{DSS}	_	_	1	μAdc
Gate-Source Leakage Current (V _{GS} = 10 Vdc, V _{DS} = 0 Vdc)	I _{GSS}	_	_	1	μAdc
On Characteristics					
Gate Threshold Voltage (V_{DS} = 12.5 Vdc, I_D = 60 μ A)	V _{GS(th)}	1	1.7	2.1	Vdc
Drain-Source On-Voltage (V _{GS} = 10 Vdc, I _D = 500 mAdc)	V _{DS(on)}	_	0.65	_	Vdc
Dynamic Characteristics	<u> </u>				
Input Capacitance $(V_{DS} = 12.5 \text{ Vdc}, V_{GS} = 0, f = 1 \text{ MHz})$	C _{iss}	_	33	_	pF
Output Capacitance (V _{DS} = 12.5 Vdc, V _{GS} = 0, f = 1 MHz)	C _{oss}	_	16.5	_	pF
Reverse Transfer Capacitance (V _{DS} = 12.5 Vdc, V _{GS} = 0, f = 1 MHz)	C _{rss}	_	2.2	_	pF
Functional Tests (In Freescale Test Fixture)	•	•	•	•	•
Common-Source Amplifier Power Gain (V _{DD} = 12.5 Vdc, P _{out} = 3 Watts, I _{DQ} = 50 mA, f = 520 MHz)	G _{ps}	_	15	_	dB
Drain Efficiency $(V_{DD} = 12.5 \text{ Vdc}, P_{out} = 3 \text{ Watts}, I_{DQ} = 50 \text{ mA}, f = 520 \text{ MHz})$	η	_	65	_	%

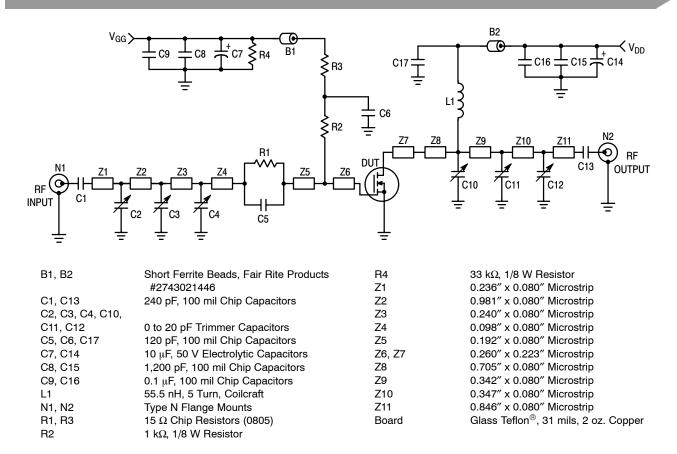


Figure 1. 450 - 520 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 450 - 520 MHz

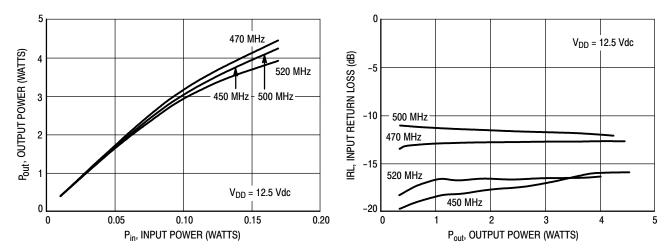


Figure 2. Output Power versus Input Power

Figure 3. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 450 - 520 MHz

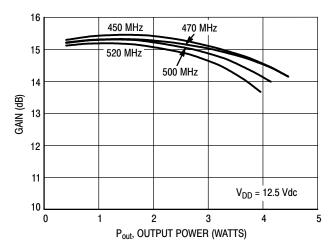


Figure 4. Gain versus Output Power

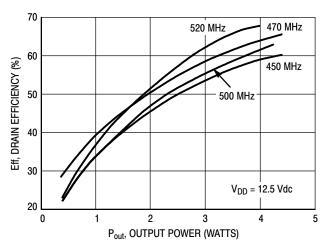


Figure 5. Drain Efficiency versus Output Power

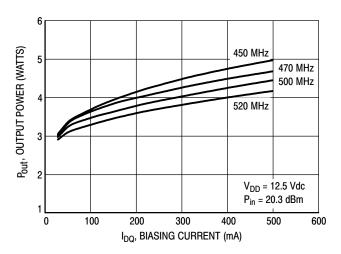


Figure 6. Output Power versus Biasing Current

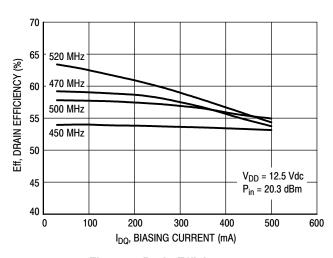


Figure 7. Drain Efficiency versus
Biasing Current

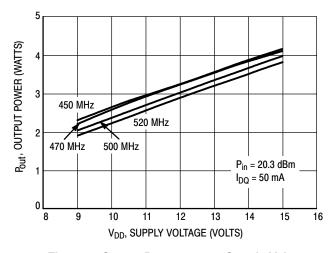


Figure 8. Output Power versus Supply Voltage

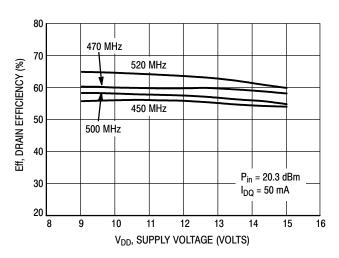


Figure 9. Drain Efficiency versus Supply Voltage

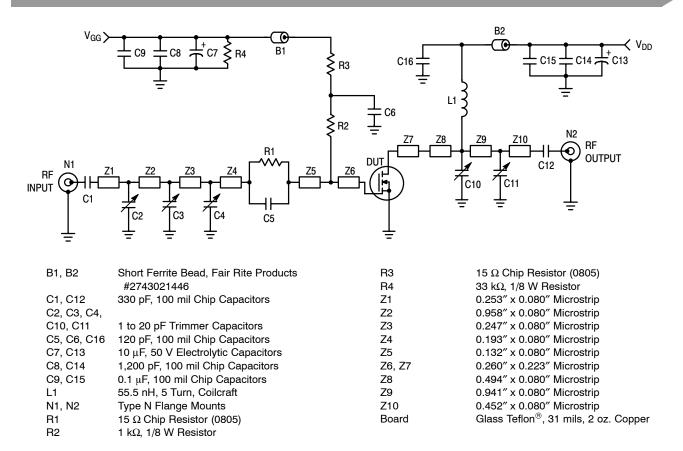
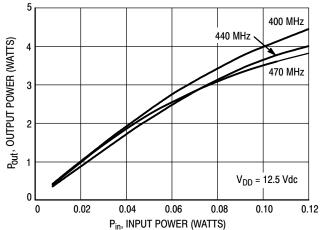
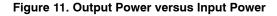


Figure 10. 400 - 470 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 400 - 470 MHz





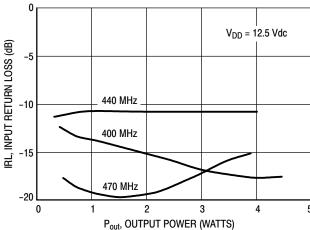


Figure 12. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 400 - 470 MHz

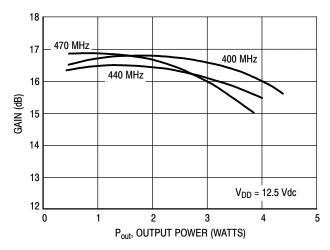


Figure 13. Gain versus Output Power

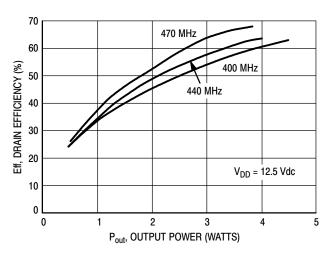


Figure 14. Drain Efficiency versus Output Power

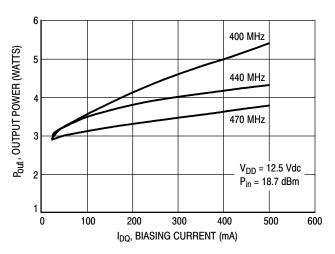


Figure 15. Output Power versus Biasing Current

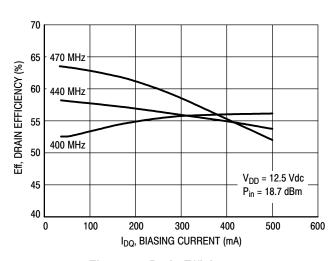


Figure 16. Drain Efficiency versus
Biasing Current

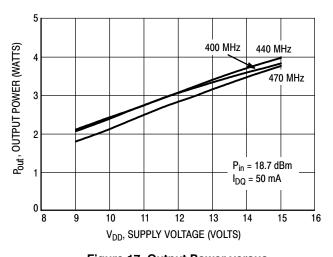


Figure 17. Output Power versus Supply Voltage

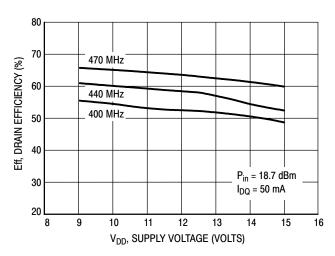


Figure 18. Drain Efficiency versus Supply Voltage

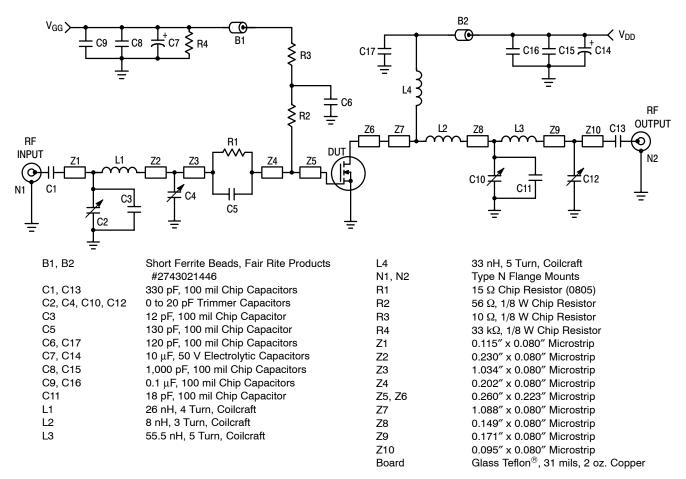


Figure 19. 135 - 175 MHz Broadband Test Circuit

TYPICAL CHARACTERISTICS, 135 - 175 MHz

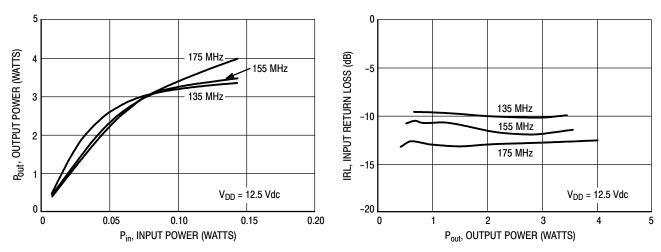


Figure 20. Output Power versus Input Power

Figure 21. Input Return Loss versus Output Power

TYPICAL CHARACTERISTICS, 135 - 175 MHz

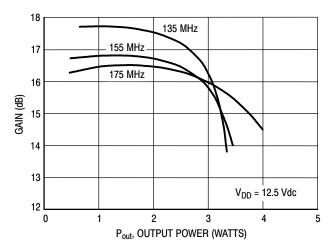


Figure 22. Gain versus Output Power

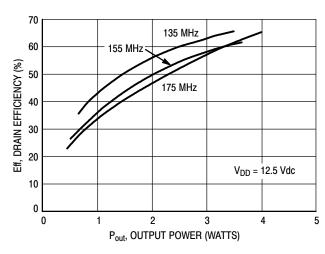


Figure 23. Drain Efficiency versus Output Power

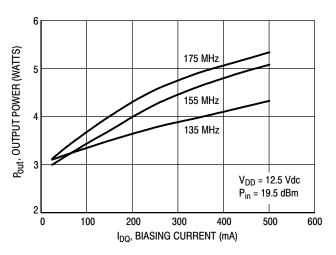


Figure 24. Output Power versus Biasing Current

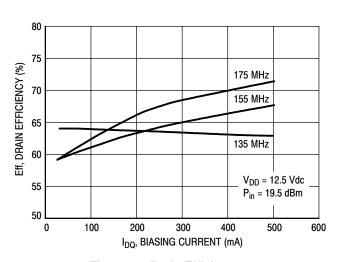


Figure 25. Drain Efficiency versus
Biasing Current

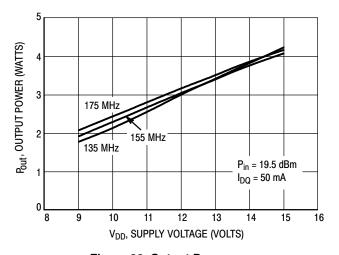


Figure 26. Output Power versus Supply Voltage

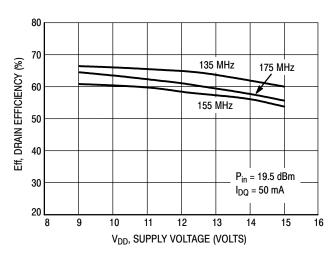
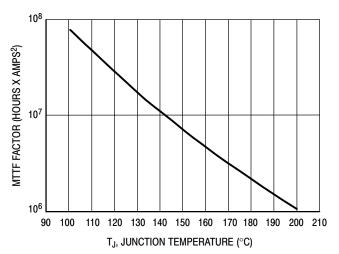


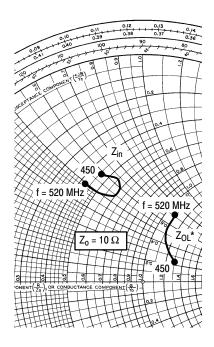
Figure 27. Drain Efficiency versus Supply Voltage

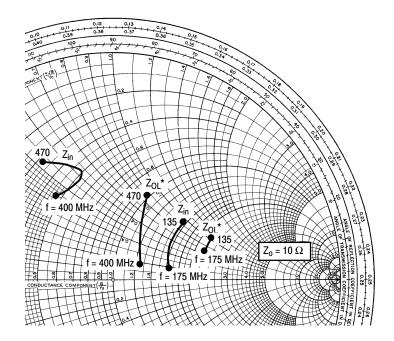
TYPICAL CHARACTERISTICS



This above graph displays calculated MTTF in hours x ampere² drain current. Life tests at elevated temperatures have correlated to better than $\pm 10\%$ of the theoretical prediction for metal failure. Divide MTTF factor by $I_D{}^2$ for MTTF in a particular application.

Figure 28. MTTF Factor versus Junction Temperature





 V_{DD} = 12.5 V, I_{DQ} = 50 mA, P_{out} = 3 W

f MHz	$\mathbf{Z_{in}}$	Z_{OL}* Ω
450	4.64 +j5.82	13.11 +j2.15
470	5.42 +j6.34	12.16 +j3.26
500	5.96 +j5.45	11.03 +j5.42
520	4.28 +j4.94	10.99 +j7.18

 $V_{DD} = 12.5 \text{ V}, I_{DQ} = 50 \text{ mA}, P_{out} = 3 \text{ W}$

f MHz	Z _{in} Ω	Z_{OL}* Ω
400	4.72 +j4.38	12.57 +j1.88
440	4.88 +j6.34	11.21 +j5.87
470	3.22 +j5.24	9.82 +j8.63

 $V_{DD} = 12.5 \text{ V}, I_{DQ} = 50 \text{ mA}, P_{out} = 3 \text{ W}$

f MHz	Z _{in} Ω	Z_{OL}* Ω
135	16.55 +j1.82	22.01 +j10.32
155	15.59 +j5.38	22.03 +j8.07
175	15.55 +j9.43	22.08 +j6.85

- Z_{in} = Complex conjugate of source impedance with parallel 15 Ω resistor and 120 pF capacitor in series with gate. (See Figure 1).
- $$\begin{split} Z_{OL}{}^{\star} &= & \text{Complex conjugate of the load} \\ & \text{impedance at given output power,} \\ & \text{voltage, frequency, and } \eta_D > 50 \text{ \%}. \end{split}$$
- $Z_{\rm in}$ = Complex conjugate of source impedance with parallel 15 Ω resistor and 130 pF capacitor in series with gate. (See Figure 10).
- $$\begin{split} Z_{OL}{}^{\star} &= & \text{Complex conjugate of the load} \\ & \text{impedance at given output power,} \\ & \text{voltage, frequency, and } \eta_D > 50 \text{ \%}. \end{split}$$
- Z_{in} = Complex conjugate of source impedance with parallel 15 Ω resistor and 130 pF capacitor in series with gate. (See Figure 19).
- Z_{OL}^* = Complex conjugate of the load impedance at given output power, voltage, frequency, and $\eta_D > 50$ %.

Note: Z_{OL}^* was chosen based on tradeoffs between gain, drain efficiency, and device stability.

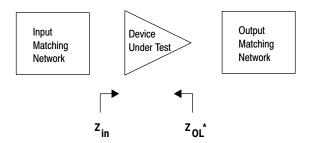


Figure 29. Series Equivalent Input and Output Impedance

Table 5. Common Source Scattering Parameters (V_{DD} = 12.5 Vdc)

$I_{DQ} = 50 \text{ mA}$

f	s	11	S	21	s	12	s	22
MHz	S ₁₁	∠ ¢	S ₂₁	∠ ¢	S ₁₂	∠ ¢	S ₂₂	∠ ¢
50	0.93	-94	22.09	125	0.044	33	0.77	-81
100	0.81	-131	12.78	101	0.052	6	0.61	-115
200	0.76	-153	6.31	81	0.047	-10	0.59	-135
300	0.76	-160	3.92	69	0.044	-19	0.64	-142
400	0.77	-164	2.74	60	0.040	-26	0.70	-147
500	0.79	-167	1.99	54	0.036	-31	0.75	-151
600	0.80	-169	1.55	48	0.034	-37	0.80	-155
700	0.81	-171	1.25	44	0.028	-40	0.82	-158
800	0.82	-172	1.02	38	0.027	-42	0.86	-161
900	0.83	-173	0.85	35	0.017	-42	0.88	-163
1000	0.84	-175	0.70	29	0.018	-49	0.91	-166

$I_{DQ} = 500 \text{ mA}$

f	s	11	S	S ₂₁		12	s	22
MHz	S ₁₁	∠ ¢	S ₂₁	∠ ¢	S ₁₂	∠¢	S ₂₂	∠ ¢
50	0.84	-127	32.57	112	0.025	17	0.64	-130
100	0.80	-152	17.23	97	0.025	13	0.64	- 153
200	0.78	-166	8.62	85	0.025	-9	0.65	-163
300	0.78	-171	5.58	79	0.023	-9	0.67	-166
400	0.78	-173	4.08	72	0.022	-9	0.69	-166
500	0.78	-175	3.14	68	0.020	-10	0.71	-167
600	0.79	-176	2.55	63	0.022	-15	0.74	-168
700	0.79	-177	2.14	60	0.019	-20	0.76	-168
800	0.80	-178	1.80	54	0.018	-31	0.79	-170
900	0.81	-178	1.54	51	0.015	-25	0.80	-170
1000	0.82	-179	1.31	46	0.012	-36	0.81	-172

$I_{DQ} = 1 A$

f	s	11	S	21	S	12	s	22
MHz	S ₁₁	∠ф	S ₂₁	∠ φ	S ₁₂	∠¢	S ₂₂	∠¢
50	0.84	-129	32.57	111	0.023	24	0.61	-137
100	0.80	-153	17.04	97	0.024	13	0.64	-156
200	0.78	-167	8.52	85	0.023	5	0.65	-165
300	0.77	-172	5.53	79	0.020	-7	0.67	-167
400	0.77	-174	4.06	73	0.020	-11	0.69	-167
500	0.78	-175	3.13	69	0.021	-9	0.72	-167
600	0.78	-177	2.54	64	0.017	-26	0.74	-168
700	0.78	-177	2.13	60	0.017	-14	0.75	-168
800	0.79	-178	1.81	55	0.015	-23	0.78	-170
900	0.80	-178	1.54	51	0.013	-31	0.79	-170
1000	0.80	-179	1.30	46	0.011	-17	0.80	-172

APPLICATIONS INFORMATION

DESIGN CONSIDERATIONS

This device is a common-source, RF power, N-Channel enhancement mode, Lateral Metal-Oxide Semiconductor Field-Effect Transistor (MOSFET). Freescale Application Note AN211A, "FETs in Theory and Practice", is suggested reading for those not familiar with the construction and characteristics of FETs.

This surface mount packaged device was designed primarily for VHF and UHF portable power amplifier applications. Manufacturability is improved by utilizing the tape and reel capability for fully automated pick and placement of parts. However, care should be taken in the design process to insure proper heat sinking of the device.

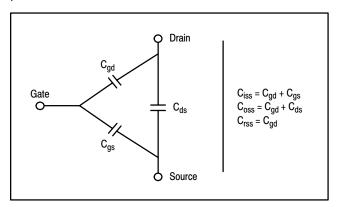
The major advantages of Lateral RF power MOSFETs include high gain, simple bias systems, relative immunity from thermal runaway, and the ability to withstand severely mismatched loads without suffering damage.

MOSFET CAPACITANCES

The physical structure of a MOSFET results in capacitors between all three terminals. The metal oxide gate structure determines the capacitors from gate-to-drain (C_{gd}), and gate-to-source (C_{gs}). The PN junction formed during fabrication of the RF MOSFET results in a junction capacitance from drain-to-source (C_{ds}). These capacitances are characterized as input (C_{iss}), output (C_{oss}) and reverse transfer (C_{rss}) capacitances on data sheets. The relationships between the inter-terminal capacitances and those given on data sheets are shown below. The C_{iss} can be specified in two ways:

- 1. Drain shorted to source and positive voltage at the gate.
- Positive voltage of the drain in respect to source and zero volts at the gate.

In the latter case, the numbers are lower. However, neither method represents the actual operating conditions in RF applications.



DRAIN CHARACTERISTICS

One critical figure of merit for a FET is its static resistance in the full-on condition. This on-resistance, $R_{DS(on)}$, occurs in the linear region of the output characteristic and is specified at a specific gate-source voltage and drain current. The

drain-source voltage under these conditions is termed $V_{DS(on)}$. For MOSFETs, $V_{DS(on)}$ has a positive temperature coefficient at high temperatures because it contributes to the power dissipation within the device.

 ${\rm BV_{DSS}}$ values for this device are higher than normally required for typical applications. Measurement of ${\rm BV_{DSS}}$ is not recommended and may result in possible damage to the device.

GATE CHARACTERISTICS

The gate of the RF MOSFET is a polysilicon material, and is electrically isolated from the source by a layer of oxide. The DC input resistance is very high - on the order of $10^9~\Omega$ — resulting in a leakage current of a few nanoamperes.

Gate control is achieved by applying a positive voltage to the gate greater than the gate-to-source threshold voltage, $V_{\rm GS(th)}$.

Gate Voltage Rating — Never exceed the gate voltage rating. Exceeding the rated V_{GS} can result in permanent damage to the oxide layer in the gate region.

Gate Termination — The gates of these devices are essentially capacitors. Circuits that leave the gate open-circuited or floating should be avoided. These conditions can result in turn-on of the devices due to voltage build-up on the input capacitor due to leakage currents or pickup.

Gate Protection — These devices do not have an internal monolithic zener diode from gate-to-source. If gate protection is required, an external zener diode is recommended. Using a resistor to keep the gate-to-source impedance low also helps dampen transients and serves another important function. Voltage transients on the drain can be coupled to the gate through the parasitic gate-drain capacitance. If the gate-to-source impedance and the rate of voltage change on the drain are both high, then the signal coupled to the gate may be large enough to exceed the gate-threshold voltage and turn the device on.

DC BIAS

Since this device is an enhancement mode FET, drain current flows only when the gate is at a higher potential than the source. RF power FETs operate optimally with a quiescent drain current (I_{DQ}), whose value is application dependent. This device was characterized at $I_{DQ} = 50$ mA, which is the suggested value of bias current for typical applications. For special applications such as linear amplification, I_{DQ} may have to be selected to optimize the critical parameters.

The gate is a dc open circuit and draws no current. Therefore, the gate bias circuit may generally be just a simple resistive divider network. Some special applications may require a more elaborate bias system.

GAIN CONTROL

Power output of this device may be controlled to some degree with a low power dc control signal applied to the gate, thus facilitating applications such as manual gain control, ALC/AGC and modulation systems. This characteristic is very dependent on frequency and load line.

MOUNTING

The specified maximum thermal resistance of 4°C/W assumes a majority of the $0.065'' \times 0.180''$ source contact on the back side of the package is in good contact with an appropriate heat sink. As with all RF power devices, the goal of the thermal design should be to minimize the temperature at the back side of the package. Refer to Freescale Application Note AN4005/D, "Thermal Management and Mounting Method for the PLD-1.5 RF Power Surface Mount Package" for additional information.

AMPLIFIER DESIGN

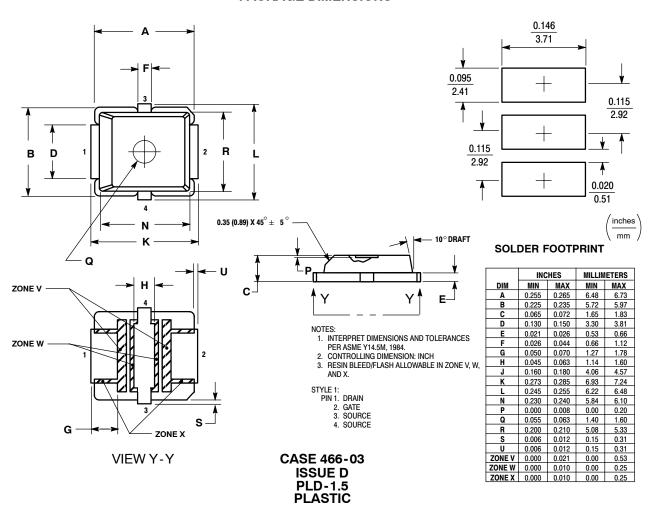
Impedance matching networks similar to those used with bipolar transistors are suitable for this device. For examples see Freescale Application Note AN721, "Impedance Matching Networks Applied to RF Power Transistors." Large-signal impedances are provided, and will yield a good

first pass approximation.

Since RF power MOSFETs are triode devices, they are not unilateral. This coupled with the very high gain of this device yields a device capable of self oscillation. Stability may be achieved by techniques such as drain loading, input shunt resistive loading, or output to input feedback. The RF test fixture implements a parallel resistor and capacitor in series with the gate, and has a load line selected for a higher efficiency, lower gain, and more stable operating region.

Two-port stability analysis with this device's S-parameters provides a useful tool for selection of loading or feedback circuitry to assure stable operation. See Freescale Application Note AN215A, "RF Small-Signal Design Using Two-Port Parameters" for a discussion of two port network theory and stability.

PACKAGE DIMENSIONS



PRODUCT DOCUMENTATION

Refer to the following documents to aid your design process.

Application Notes

- AN211A: Field Effect Transistors in Theory and Practice
- AN215A: RF Small-Signal Design Using Two-Port Parameters
- AN721: Impedance Matching Networks Applied to RF Power Transistors
- AN4005: Thermal Management and Mounting Method for the PLD 1.5 RF Power Surface Mount Package

Engineering Bulletins

• EB212: Using Data Sheet Impedances for RF LDMOS Devices

REVISION HISTORY

The following table summarizes revisions to this document.

Revision	Date	Description
10	Feb. 2008	Changed DC Bias I _{DQ} value from 150 to 50 to match Functional Test I _{DQ} specification, p. 12 Added Product Decumentation and Provision History p. 15
		Added Product Documentation and Revision History, p. 15

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